



ASSEMBLY — 40TH SESSION

TECHNICAL COMMISSION

Agenda Item 30: Other issues to be considered by the Technical Commission

SAFETY EVALUATION OF CONVERSION FACTOR (K) IN TEHRAN TMA

(Presented by Iran (Islamic Republic of))

EXECUTIVE SUMMARY

Conversion factor (K) is an agent that is related to temperature and altitude. It is used in conversion calculating indicated air speed (IAS) to true airspeed (TAS). In *Procedures for Air Navigation Services — Aircraft Operations* (PANS-OPS, Doc 8168), $ISA + 15^{\circ}C$ is used as an instance, but this document has mentioned several times that the domestic information should be used not $ISA + 15^{\circ}C$. If conversion factor (K) calculating is used correctly, it causes flight safety to increase. It is important that procedure designers elect temperature correctly and with regard to relationship “K” to ISA; if the procedure is not designed correctly, this can result in significant differences in the tracks that the aircraft fly. For designing procedures, the worst case conditions of maximum and minimum temperatures that could prevail should be considered.

| | |
|--------------------------------|---|
| <i>Strategic Objectives:</i> | This working paper relates to the Safety Strategic Objective. |
| <i>Financial implications:</i> | N/A |
| <i>References:</i> | Doc 8400, <i>Procedures for Air Navigation Services — ICAO Abbreviations and Codes</i> (PANS-ABC) Doc 8168, <i>Procedures for Air Navigation Services — Aircraft Operations</i> (PANS-OPS) IMO, Iranian Meteorological Organization |

1. INTRODUCTION

1.1 Conversion factor (K) is an agent that is related to temperature and altitude. It is used in conversion calculating IAS to TAS. In PANS-OPS, $ISA+15^{\circ}C$ is used as an instance, but this document has mentioned several times that the domestic information should be used not the $ISA+15^{\circ}C$. If conversion factor (K) calculating is used correctly, it causes flight safety to increase. (Formula (1) and (2))

$$K = 171233 * [(288 \pm VAR) - 0.00198H]^{0.5} \div (288 - 0.00198H)^{2.628} \quad (1)$$

$$K = 171233 * [(288 \pm VAR) - 0.006496h]^{0.5} \div (288 - 0.006496h)^{2.628} \quad (2)$$

That H (altitude) by feet, h (altitude) by feet and VAR (temperature variable) is by degrees centigrade. [2]

1.2 An important aspect for procedure designers is elect temperature correctly and with regard to relationship “K” to ISA; if the procedure is not designed correctly, this can result in significant differences in the tracks that the aircraft fly.

1.3 For designing procedures, the worst-case conditions of maximum and minimum temperatures that could prevail should be considered. [2]

2. INFLUENCE OF CONVERSION FACTOR (K) ON THE OTHER SECTIONS

2.1 Speed (IAS, TAS)

In all design calculating, suppose speed based on TAS authorized. (Formula (3) and (4) [2])

$$TAS = V = IAS * K \quad (3)$$

$$TAS = 55.1085\sqrt{T} \sqrt{1 + 0.0023157 \frac{IAS^2}{P} \left(1 + \frac{IAS^2}{1750200}\right) - 1} \quad \text{or} \quad (4)$$

That T (temperature) is by Kelvin in $ISA+15^{\circ}C$ and P (pressure) is by Hectopascal.

2.2 Importance of temperature (Temp) [2]

2.2.1 Considering the fact that conversion factor (K) is variable in different altitudes and temperatures, in every area for designing flight procedure minimum and maximum averages are needed. In below instances, for presentation of flight procedures, and using minimum speed authorized minimum temperature average in that area is needed; in PANS-OPS examples, $ISA-10^{\circ}C$ is used:

- a) missed approach;
- b) minimum speed in final; and
- c) minimum speed in MAPt tolerance.

2.2.2 Thus, for presentation of flight maximum speed authorized, maximum temperature average of that area is needed; in PANS-OPS examples, $ISA + 15^{\circ}C$ is used:

- a) departure segment;
- b) missed approach segment for maximum speed especially in turning;
- c) missed approach segment for precision procedures;
- d) maximum speed in final; and
- e) maximum speed in missed approach tolerance.

2.2.3 In earliest and latest MAPt, MAPt to SOC distance calculating:

- f) visual manoeuvring area;
- g) global navigation satellite system (GNSS) arrival;
- h) racetrack and reversal procedure area;
- i) waypoint tolerance (ATT and XTT);
- j) HLDG and RNP HLDG procedure; and
- k) TAS in AWY.

Need for conversion for IAS to TAS with regard to Table III-1-1 and 2 from PANS-OPS.

2.2.4 With regard to instances of descript use of conversion factor (K) in conversion IAS to TAS, conversion factor (K) importance is perfectly clear and this factor in Iran area should be calculated and used with high accuracy.

3. AVERAGE EVALUATION OF TEMPERATURE MIN AND MAX

3.1 After minimum and maximum temperature value analysis (from Tehran synoptic station in pressure level 850 mbar to 400 mbar (below 19 500 ft) between 1986 up to 2015 (30 years)), below quantities prepared.

3.2 Table 1 is representation of maximum temperature up to 400 mbar (19 500 ft) that maximum temperature reported $+37.4^{\circ}C$ in July 1998 and in Table 2 annual maximum temperature average with $+18.35^{\circ}C$ value is calculated and thus Table 3 is representation of minimum temperature from surface up to 850 mbar (5 000 ft) that minimum temperature reported $-7.7^{\circ}C$ in March 1987 and in Table 4 annual minimum temperature average with $+16.22^{\circ}C$ value is calculated.

3.3 Results of calculating show that maximum temperature in hot months up to 400 mbar in 1986 up to 2015 (30 years) was $+25.64^{\circ}C$ that with 95 per cent confidence coefficient was $+26.4^{\circ}C$

(Table 5) and that minimum temperature in cold months up to 850 mbar in 1986 up to 2015 (30 years) was + 6.24^{°C} that with 95 per cent confidence coefficient was + 5.84^{°C} (Table 6).

3.4 Graph 1 is representation of annual average changes of maximum (MAX) temperature (in year hot months) in pressure level 400 mbar and minimum (MIN) temperature (in year cold months) in pressure level 850 mbar in 1986 to 2015. [1]

Table 1 – Annual changes of MAX Temp in pressure level 400 mbar in 1986 to 2015

| MAX Temperature (Degrees) | | | |
|---------------------------|----------|------|----------|
| Years : 1986 Until 2015 | | | |
| Year | MAX Temp | Year | MAX Temp |
| 1986 | 35.50 | 2001 | 36.30 |
| 1987 | 35.90 | 2002 | 35.30 |
| 1988 | 35.00 | 2003 | 34.80 |
| 1989 | 35.07 | 2004 | 35.30 |
| 1990 | 33.80 | 2005 | 36.50 |
| 1991 | 36.60 | 2006 | 35.10 |
| 1992 | 36.00 | 2007 | 35.20 |
| 1993 | 33.60 | 2008 | 36.10 |
| 1994 | 33.80 | 2009 | 34.20 |
| 1995 | 36.20 | 2010 | 35.90 |
| 1996 | 36.00 | 2011 | 37.00 |
| 1997 | 34.60 | 2012 | 34.70 |
| 1998 | 35.50 | 2013 | 36.80 |
| 1999 | 37.40 | 2014 | 26.50 |
| 2000 | 30.80 | 2015 | 14.40 |
| Results (1986 Until 2015) | | | |
| MAX (Jull 83) | | | 37.40 |

Table 2–Annual average changes of MAX Temp in pressure level 400 mbar in 1986 to 2015

| MAX Temperature average (Degrees) | | | |
|-----------------------------------|----------|------|----------|
| Years : 1986 Until 2015 | | | |
| Year | MAX Temp | Year | MAX Temp |
| 1986 | 18.61 | 2001 | 18.65 |
| 1987 | 18.09 | 2002 | 17.68 |
| 1988 | 15.95 | 2003 | 18.65 |
| 1989 | 17.66 | 2004 | 18.67 |
| 1990 | 16.57 | 2005 | 18.99 |
| 1991 | 17.35 | 2006 | 19.10 |
| 1992 | 16.90 | 2007 | 18.03 |
| 1993 | 15.85 | 2008 | 19.73 |
| 1994 | 22.19 | 2009 | 17.18 |
| 1995 | 22.08 | 2010 | 17.71 |
| 1996 | 27.54 | 2011 | 21.00 |
| 1997 | 20.39 | 2012 | 22.85 |
| 1998 | 16.86 | 2013 | 18.59 |
| 1999 | 17.98 | 2014 | 13.75 |
| 2000 | 14.85 | 2015 | 11.55 |
| Results (1986 Until 2015) | | | |
| Average | | | 18.37 |

Table 3 – Annual changes of MIN Temp in pressure level 850 mbar in 1986 to 2015

| MIN Temperature (Degrees) | | | |
|---------------------------|----------|------|----------|
| Years : 1986 Until 2015 | | | |
| Year | MIN Temp | Year | MIN Temp |
| 1986 | 0.50 | 2001 | 2.60 |
| 1987 | 1.6 | 2002 | 2.10 |
| 1988 | -7.7 | 2003 | 4.90 |
| 1989 | -3.3 | 2004 | 2.00 |
| 1990 | -2.3 | 2005 | -0.90 |
| 1991 | -2.1 | 2006 | 0.60 |
| 1992 | -0.1 | 2007 | 1.70 |
| 1993 | -3.6 | 2008 | 0.40 |
| 1994 | 7.2 | 2009 | 0.30 |
| 1995 | 6.5 | 2010 | 2.10 |
| 1996 | 16.9 | 2011 | 4.90 |
| 1997 | 4.9 | 2012 | 7.20 |
| 1998 | -0.3 | 2013 | 0.50 |
| 1999 | -0.8 | 2014 | 0.50 |
| 2000 | -0.6 | 2015 | 8.70 |
| Results (1986 Until 2015) | | | |
| MIN (MAR 72) | | | -7.70 |

Table 4 – Annual average changes of MIN Temp in pressure level 850 mbar in 1986 to 2015

| MIN Temperature average (Degrees) | | | |
|-----------------------------------|----------|------|----------|
| Years : 1986 Until 2015 | | | |
| Year | MIN Temp | Year | MIN Temp |
| 1986 | 16.98 | 2001 | 16.26 |
| 1987 | 16.34 | 2002 | 15.73 |
| 1988 | 13.47 | 2003 | 16.52 |
| 1989 | 15.74 | 2004 | 16.90 |
| 1990 | 14.77 | 2005 | 16.08 |
| 1991 | 15.42 | 2006 | 17.17 |
| 1992 | 14.82 | 2007 | 15.99 |
| 1993 | 14.32 | 2008 | 15.70 |
| 1994 | 20.33 | 2009 | 14.53 |
| 1995 | 20.28 | 2010 | 15.67 |
| 1996 | 25.52 | 2011 | 18.85 |
| 1997 | 18.07 | 2012 | 20.82 |
| 1998 | 15.33 | 2013 | 14.67 |
| 1999 | 16.32 | 2014 | 11.49 |
| 2000 | 12.94 | 2015 | 09.65 |
| Results (1986 Until 2015) | | | |
| Average | | | 16.22 |

Table 5 – Annual average changes of MAX Temp (in year hot months) in pressure level 400 mbar in 1986 to 2015

| MAX Temperature average (Degrees) | | | |
|-----------------------------------|----------|------|----------|
| Years : 1986 Until 2015 | | | |
| Year | MAX Temp | Year | MAX Temp |
| 1986 | 25.52 | 2001 | 26.04 |
| 1987 | 24.92 | 2002 | 24.99 |
| 1988 | 24.37 | 2003 | 24.97 |
| 1989 | 25.19 | 2004 | 25.77 |
| 1990 | 24.14 | 2005 | 26.99 |
| 1991 | 25.34 | 2006 | 26.62 |
| 1992 | 25.63 | 2007 | 25.54 |
| 1993 | 23.70 | 2008 | 27.27 |
| 1994 | 27.20 | 2009 | 25.22 |
| 1995 | 28.28 | 2010 | 24.39 |
| 1996 | 27.54 | 2011 | 25.75 |
| 1997 | 25.06 | 2012 | 27.61 |
| 1998 | 25.09 | 2013 | 25.82 |
| 1999 | 25.67 | 2014 | 26.15 |
| 2000 | 22.80 | 2015 | -- |
| Results (1986 Until 2015) | | | |
| Average | | | 25.64 |
| Average 95% Confidence-MAX | | | 26.4 |

Table 6 – Annual average changes of MIN Temp (in year cold months) in pressure level 850 mbar in 86-15

| MIN Temperature average (Degrees) | | | |
|-----------------------------------|----------|------|----------|
| Years : 1986 Until 2015 | | | |
| Year | MIN Temp | Year | MIN Temp |
| 1986 | 7.44 | 2001 | 6.63 |
| 1987 | 7.00 | 2002 | 5.75 |
| 1988 | 0.91 | 2003 | 8.08 |
| 1989 | 5.37 | 2004 | 7.22 |
| 1990 | 4.32 | 2005 | 5.21 |
| 1991 | 3.95 | 2006 | 6.84 |
| 1992 | 4.35 | 2007 | 5.73 |
| 1993 | 6.78 | 2008 | 5.64 |
| 1994 | 8.43 | 2009 | 4.43 |
| 1995 | 10.38 | 2010 | 7.00 |
| 1996 | -- | 2011 | 7.93 |
| 1997 | 9.33 | 2012 | 8.83 |
| 1998 | 4.35 | 2013 | 5.72 |
| 1999 | 5.76 | 2014 | 2.67 |
| 2000 | 5.15 | 2015 | 9.55 |
| Results (1986 Until 2015) | | | |
| Average | | | 6.24 |
| Average 95% Confidence - MIN | | | 5.84 |

4. RESULTS AND RECOMMENDATION FOR INCREASING SAFETY

4.1 Table 7 represents an increase if safety coefficient is in different altitudes. For example, for IAS=220 kts, ALT =10 000 ft, $K^{+15}=1.1958$, S will be 263 kts but if we do new value $K^{+26.4}=1.2192$, TAS will be 268 kts that in this situation for use of TAS, **safety coefficient (K) increases by 2%**. It is worthy of mention with regard to increase the aforementioned safety coefficient **increases by 2%** in Iran.

Table 7. Percentage of conversion factor (K) increase (Non-SI units)

| (ALT-ft) | K | K | K | K | Increase of Safety 15° to 26.4° (%) |
|----------|---------|--------|---------|-----------|--|
| | ISA -10 | ISA +5 | ISA +15 | ISA +26.4 | K% |
| 0 | 0.9825 | 1.0086 | 1.0257 | 1.0448 | 1.9 |
| 1000 | 1.0165 | 1.0236 | 1.0411 | 1.0606 | 1.9 |
| 2000 | 1.0317 | 1.0389 | 1.0567 | 1.0767 | 1.9 |
| 3000 | 1.0473 | 1.0546 | 1.0728 | 1.0932 | 1.9 |
| 4000 | 1.0631 | 1.0706 | 1.0892 | 1.1100 | 1.9 |
| 5000 | 1.0793 | 1.0869 | 1.1059 | 1.1273 | 1.9 |
| 10000 | 1.1662 | 1.1745 | 1.1958 | 1.2196 | 2.0 |
| 11000 | 1.1847 | 1.1932 | 1.2150 | 1.2394 | 2.0 |
| 12000 | 1.2038 | 1.2124 | 1.2347 | 1.2597 | 2.0 |
| 14000 | 1.2432 | 1.2522 | 1.2755 | 1.3017 | 2.0 |
| 15000 | 1.2637 | 1.2728 | 1.2967 | 1.3235 | 2.1 |
| 20000 | 1.3737 | 1.3837 | 1.4107 | 1.4409 | 2.1 |
| 21000 | 1.3974 | 1.4075 | 1.4353 | 1.4662 | 2.2 |
| 22000 | 1.4217 | 1.4320 | 1.4605 | 1.4922 | 2.2 |
| 23000 | 1.4466 | 1.4572 | 1.4863 | 1.5189 | 2.2 |
| 24000 | 1.4722 | 1.4829 | 1.5128 | 1.5462 | 2.2 |

4.2 With regard to instances mentioned in PANS-OPS and Tables III-F-1 and III-F-2, the minimum temperature average ($+5^{\circ}\text{C}$) with confidence coefficient and maximum temperature average ($+26.4^{\circ}\text{C}$) with confidence coefficient finally, will result in Tables 8 and 9, which **will replace Tables III-F-1 and III-F-2** (from PANS-OPS) for use in Iran. [1][2]

| Table 8 – Conversion table for IAS to TAS calculations (Non-SI units) | | | | |
|--|---------|--------|---------|-----------|
| Replace to Table III-F-2 for use in Iran | | | | |
| Conversion factor | | | | |
| Altitude (Ft) | ISA -10 | ISA +5 | ISA +15 | ISA +26.4 |
| 0.0 | 0.9825 | 1.0086 | 1.0257 | 1.0448 |
| 1000.0 | 1.0165 | 1.0236 | 1.0411 | 1.0606 |
| 2000.0 | 1.0317 | 1.0389 | 1.0567 | 1.0767 |
| 4000.0 | 1.0631 | 1.0706 | 1.0892 | 1.1100 |
| 6000.0 | 1.0959 | 1.1036 | 1.1231 | 1.1449 |
| 8000.0 | 1.1302 | 1.1382 | 1.1586 | 1.1814 |
| 10000.0 | 1.1662 | 1.1745 | 1.1958 | 1.2196 |
| 11000.0 | 1.1847 | 1.1932 | 1.2150 | 1.2394 |
| 12000.0 | 1.2038 | 1.2124 | 1.2347 | 1.2597 |
| 14000.0 | 1.2432 | 1.2522 | 1.2755 | 1.3017 |
| 15000.0 | 1.2637 | 1.2728 | 1.2967 | 1.3235 |
| 16000.0 | 1.2846 | 1.2939 | 1.3184 | 1.3458 |
| 18000.0 | 1.3280 | 1.3377 | 1.3634 | 1.3922 |
| 20000.0 | 1.3737 | 1.3837 | 1.4107 | 1.4409 |
| 22000.0 | 1.4217 | 1.4320 | 1.4605 | 1.4922 |
| 24000.0 | 1.4722 | 1.4829 | 1.5128 | 1.5462 |

| Table 9 – Conversion table for IAS to TAS calculations (SI units) | | | | |
|--|---------|--------|---------|-----------|
| Replace to Table III-F-1 for use in Iran | | | | |
| Conversion factor | | | | |
| Altitude (m) | ISA -10 | ISA +5 | ISA +15 | ISA +26.4 |
| 0.0 | 0.9825 | 1.0086 | 1.0257 | 1.0448 |
| 500.0 | 1.0262 | 1.0334 | 1.0511 | 1.0709 |
| 1000.0 | 1.0517 | 1.0590 | 1.0774 | 1.0979 |
| 1500.0 | 1.0780 | 1.0856 | 1.1046 | 1.1259 |
| 2000.0 | 1.1054 | 1.1132 | 1.1329 | 1.1550 |
| 2500.0 | 1.1338 | 1.1418 | 1.1623 | 1.1851 |
| 3000.0 | 1.1632 | 1.1715 | 1.1928 | 1.2165 |
| 3500.0 | 1.1939 | 1.2024 | 1.2245 | 1.2491 |
| 4000.0 | 1.2257 | 1.2345 | 1.2574 | 1.2830 |
| 4500.0 | 1.2588 | 1.2679 | 1.2917 | 1.3183 |
| 5000.0 | 1.2932 | 1.3026 | 1.3273 | 1.3550 |
| 5500.0 | 1.3290 | 1.3387 | 1.3644 | 1.3932 |
| 6000.0 | 1.3663 | 1.3763 | 1.4031 | 1.4331 |
| 6500.0 | 1.4052 | 1.4154 | 1.4434 | 1.4746 |
| 7000.0 | 1.4457 | 1.4563 | 1.4854 | 1.5179 |
| 7500.0 | 1.4879 | 1.4989 | 1.5292 | 1.5632 |

5. CONCLUSION

5.1 The Assembly is invited to advise States for evaluation of conversion factor (k) in all their country airspace for increasing safety coefficient.

— END —